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The product of parameters "d Δ n" of the liquid crystal layer 119 is set in the range of 450-550 nm. The liquid crystal material of U.S. Pat. No. 5,184,236 is left handed as defined in the art. The aligning direction of the rear orientation film on the light incident side of the liquid crystal layer 109 is a rubbing direction A_0 inclined at approximately 45° with respect to the side of the liquid crystal cell. The aligning direction of the orientation or buffing film on the front side of the liquid crystal layer is oriented in direction A_1 which is rotated about 90° in a counterclockwise direction from the orientation direction A_0 of the orientation film on the rear side of the liquid crystal material. Therefore, the liquid crystal layer 119 sandwiched between the opposing orientation films is twisted substantially 90°. The pretilting angle of the liquid crystal molecules is approximately 1°.

The rear linear polarizer 111 has a transmission axis P_1 which is parallel to the orientation direction A_0 , while the front polarizer 112 has a transmission axis direction P_2 which is parallel to the front orientation direction A_1 . The transmission axes of the front and rear polarizers 112 and 111 are perpendicular to one another thereby defining a normally white liquid crystal display. The rear retardation plate or film 113 is so arranged that its optical axis R_1 is either parallel to or crosses at 90° to the rear rubbing direction A_0 . The front retardation film 114 is so arranged that its optical axis R_2 is either parallel to or crosses at 90° to the rubbing direction A_1 . These retardation films 113 and 114 are formed to have equal retardation values (d Δ n) where "d" is the thickness of the retardation film and " Δ n" is the anisotropic or birefringent value of the retardation film. The retardation values of the retardation films 113 and 114 are set in the range of 300-400 nm. The front and rear retardation films are formed of the same material such as, for example, a polycarbonate or polyvinyl alcohol, and the outer surfaces thereof are preferably covered with a protective film made of triacetyl cellulose or the like.

The orientation or buffing directions of prior art FIG. 4 are "six o'clock buffed." The term "six o'clock buffed" means that the rear and front orientation directions A_0 and A_1 are oriented in directions so as to provide a viewing zone having an extended region in the six o'clock area of the graphs shown in FIGS. 5A-5D. In other words, because the orientation direction A_0 goes from the upper left to the lower right as shown in FIG. 4, and orientation direction A_1 goes from lower left to upper right, the resulting viewing zone has better contrast as shown in FIGS. 5A-5D in the negative vertical region below the 0° vertical viewing axis. This is what is meant by the phrase "six o'clock buffed."

Alternatively, if the orientation direction A_0 went from the lower right to the upper left, and the orientation direction A_1 was directed from the upper right to the lower left, then the display of FIG. 4 would have been "twelve o'clock buffed" and would have provided a viewing zone having better contrast ratios in the positive vertical viewing angles instead of the negative vertical viewing angles. The six o'clock buffed LCDs of FIGS. 4 and 5A-5D illustrate viewing zones with better contrast ratios in the negative vertical area below the 0° vertical viewing axis as opposed to the positive vertical viewing area above the 0° vertical viewing axis.

In the prior art liquid crystal display of FIG. 4, the contrast ratios are measured in FIGS. 5A-5D for the four possible cases of retardation film orientation, when the value of d Δ n of a liquid crystal layer 119 is set to 510 nm and the retardation value of both retardation films 113 and 114 is set to 350 nm (the value measured by the light having a wavelength of 589 nm). The four cases are as follows.

FIG. 5A shows contrast ratio curves for the case where the optical axes of the rear and front retardation films 113 and

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114 are disposed together in parallel to the rear rubbing direction A_0 . The solid or outer contrast ratio curve in FIGS. 5A-5D represents a contrast ratio of 10:1. The inner or equally broken contrast curve in FIGS. 5A-5D represents a contrast ratio of 100:1. The intermediate contrast ratio curve in FIGS. 5A-5D represents a contrast ratio of 50:1. Furthermore, in the graphs of FIGS. 5A-5D, each circle represents a 10° shift in viewing angle. In other words, the center of the graph represents a 0° vertical and 0° horizontal viewing angle, the first circle represents 10°, the second circle 20°, etc. As can be seen in FIG. 5A, the 10:1 contrast ratio curve extends horizontally along the vertical 0° viewing axis to about -37° and +40°, and extends upwardly along the 0° horizontal viewing axis to about 15° vertical.

FIG. 5B shows contrast ratio curves for the case where the optical axis R_1 of the rear retardation film 113 is disposed in parallel to the orientation direction A_0 , and the optical axis R_2 of the front retardation film 114 is disposed perpendicular to the rubbing direction A_0 . The direction R_1 is parallel to the rear polarizer axis P_1 , and R_2 is parallel to the front polarizer axis P_2 . As can be seen in FIG. 5B, the 10:1 contrast ratio curve extends along the 0° horizontal viewing axis only to about 15° vertical. Also, the 50:1 contrast ratio curve extends along the 0° horizontal viewing axis only about 5° vertical.

FIG. 5C shows contrast ratio curves for the case where the optical axes of the rear and front retardation films 113 and 114 are arranged in parallel with one another and cross at 90° to the rear rubbing direction A_0 . In FIG. 5C, the 10:1 contrast ratio curve extends upward along the 0° horizontal viewing axis only to about 15° vertical. Also, the 10:1 contrast ratio curve extends along the 0° vertical viewing axis a total of about 75°-80°.

FIG. 5D shows contrast ratio curves for the case where the optical axis R_1 of the rear retardation film 113 is arranged to cross at 90° to the rubbing direction A_0 , and the optical axis R_2 of the front retardation film 114 is arranged in parallel to rear orientation direction A_0 . In FIG. 5D, the 10:1 contrast ratio curve extends horizontally along the 0° vertical viewing axis a total of about 60°-65°. Also, the 10:1 contrast ratio curve in FIG. 5D extends upward along the 0° horizontal viewing axis only to about +15° vertical.

It was known prior to our invention to rotate retardation films to adjust the viewing zones of LCDs. For example, U.S. Pat. No. 5,184,236 teaches rotating the optical axes of retardation films $\pm 15^\circ$ or less when two such films are disposed on a single side of the liquid crystal material. The axes of the retardation films are rotated either in the clockwise or counterclockwise direction for the purpose of adjusting the viewing zone. However, when the retardation films of this patent are rotated, the symmetry of the viewing zone is substantially distorted thereby creating viewing zones which are not substantially symmetrical about the 0° horizontal viewing axis. Furthermore, this patent does not teach rotating one or both optical axes of rear and front retardation films $\pm 15^\circ$ or less for the purpose of adjusting the location of the display's viewing zone when the display includes rear and front retardation films with a liquid crystal layer therebetween.

FIG. 6 illustrates the angular relationships between the horizontal and vertical viewing axes and angles described herein relative to a liquid crystal display and conventional LCD angles ϕ and θ . The +X, +Y, and +Z axes shown in FIG. 6 are also defined in other figures herein. Furthermore, the "horizontal viewing angles" (or X_{ANG}) and "vertical viewing angles" (or Y_{ANG}) illustrated and described herein may be

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transformed to conventional LCD angles ϕ and θ by the following equations:

$$\tan(X_{\text{ANO}}) = \cos(\phi) \tan(\theta)$$

$$\sin(Y_{\text{ANO}}) = \sin(\theta) \sin(\phi)$$

or

$$\cos(\theta) = \cos(Y_{\text{ANO}}) \cos(X_{\text{ANO}})$$

$$\tan(\phi) = \tan(Y_{\text{ANO}}) \sin(X_{\text{ANO}})$$

FIGS. 7-10 are computer simulation contrast ratio curve graphs of a normally white liquid crystal display having a cell gap "d" of 5.70 μm . The display includes a rear polarizer having a transmission axis defining a first direction, a rear retardation film having an optical axis parallel to the first direction, a rear buffing zone oriented perpendicular to the first direction, a front buffing zone parallel to the first direction, a front retardation film having an optical axis perpendicular to the first direction, and a front or exit polarizer having a transmission axis perpendicular to the first direction. The retardation films are of the positively birefringent uniaxial type. This LCD of FIGS. 7-10 is not prior art to this invention but is included in this section for the purpose of later comparison with certain embodiments of this invention.

FIG. 7 is a computer simulation contrast ratio graph of the aforesaid normally white liquid crystal display wherein the wavelength of light utilized was red at 630 nm, V_{ON} was 6.8 volts, and V_{OFF} was 0.9 volts. The retardation value of both the front and rear retardation films of the display simulated in FIGS. 7-10 was 320 nm. As can be seen in FIG. 7, the 10:1 contrast ratio curve extends along the 0° vertical viewing angle from horizontal angles of about -40° to +40° thereby defining along the 0° vertical viewing axis a 10:1 total viewing zone of about 80°.

FIG. 8 is a computer simulation graph of the aforesaid display also simulated by FIG. 7. The difference between the graph of FIG. 8 and the graph of FIG. 7 is that a 5.0 V_{ON} was used as a parameter in FIG. 8. As can be seen, a reduction in V_{ON} results in a shifting upward of the viewing zone to a position centered substantially above the 0° vertical viewing axis. Also, a reduction in V_{ON} results in a vertical shrinking of the viewing zone.

FIG. 9 is a computer simulation graph illustrating the contrast ratios of the aforesaid display wherein the retardation value of the front and rear retardation films is 320 nm, and the parameter V_{ON} is 6.8 volts. The difference between the graph of FIG. 7 and the graph of FIG. 9 is that a green wavelength of 550 nm was used in FIG. 9. The reason for the higher contrast for the green wavelength as opposed to the red wavelength of FIG. 7 is that the cell gap of 5.70 μm is more nearly matched to the first transmission minimum for the green wavelength than that of the red wavelength. Accordingly, the green wavelength experiences higher contrast ratios in the center of its viewing zone. Again, the 10:1 contrast ratio curve in FIG. 9 extends horizontally along the 0° vertical viewing axis a total of about 75°.

FIG. 10 is a computer simulation graph of the aforesaid display wherein a blue wavelength of 480 nm was used. As in the graphs of FIGS. 7-9, the retardation value for the rear and front retardation films or plates was 320 nm. The 10:1 blue contrast ratio curve shown in FIG. 10 extends horizontally along the 0° vertical viewing axis a total of about 75°. The blue contrast ratio viewing zone is shifted slightly upward from that shown in FIG. 7 with respect to the red wavelength.

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As can be seen from the contrast ratio curves of FIGS. 1, 2, and 7-10, it would be highly desirable if one could provide a normally white liquid crystal display with a viewing zone including contrast ratio curves which extended to large horizontal and vertical viewing angles.

U.S. Pat. No. 4,984,874 discloses a liquid crystal display device having front and rear retardation films having retardation values of about 300 nm. A liquid crystal layer including front and rear buffing zones is sandwiched between the retardation films. The rear retardation film functions so as to convert linearly polarized light into elliptically polarized light while the front retardation film converts elliptically polarized light exiting the liquid crystal material into linear polarized light before it reaches the front or exit polarizer. The twist angle of the liquid crystal material of U.S. Pat. No. 4,984,874 is about 180°-270°.

U.S. Pat. No. 5,107,356 discloses a normally black liquid crystal display including first and second polarizers having parallel transmission axes. A liquid crystal material of this patent is sandwiched between front and rear retardation films.

While it is known to dispose rear and front 300-600 nm retardation films or plates on opposite sides of a liquid crystal layer of a P-buffed display, the prior art does not disclose providing a normally white X-buffed liquid crystal display or pixel with rear and front retardation films having 80-200 nm retardation values in order to achieve a high contrast ratio over a predetermined range of viewing angles. The prior art also does not disclose symmetrically rotating the optical axes of such rear and front retardation films so as to shift the centered position of the display's viewing zone to a point below the 0° vertical viewing axis, and thus, away from inversion areas present above the 0° vertical viewing axis.

The terms "clockwise" and "counterclockwise" as used herein mean as viewed from the viewer's or observer's side of the liquid crystal display or pixel.

The term "rear" when used herein but only as it is used to describe substrates, polarizers, electrodes, buffing zones, retardation films, and orientation films means that the described element is on the incident light side of the liquid crystal material, or in other words, on the side of the liquid crystal material opposite the viewer.

Each of the displays and light valves described herein is/was "X-buffed" unless otherwise shown or described.

The term "front" when used herein but only as it is used to describe substrates, polarizers, electrodes, buffing zones, retardation films, and orientation films means that the described element is located on the viewer side of the liquid crystal material.

The LCDs and light valves of FIGS. 1-3 and 7-45 herein include left handed liquid crystal material with a birefringence (Δn) of 0.084 at room temperature.

The term "retardation value" as used herein means " $d\Delta n$ " of the retardation film or plate, wherein "d" is the film thickness and " Δn " is the film birefringence (either positive or negative).

The term "interior" when used herein to describe a surface or side of an element, means the side or surface closest to the liquid crystal material.

The term "light valve" as used herein means a liquid crystal display pixel including: a rear polarizer, a rear retardation film (unless otherwise specified), a rear transparent substrate, a rear continuous electrode, a rear orientation film, a LC layer, a front orientation film, a front continuous pixel electrode, a front substrate, a front retardation film (unless otherwise specified), and a front polarizer in that order,

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without the presence of color filters and driving active matrix circuitry such as TFTs.

The term "contrast ratio" as used herein means the transmission of light through the display or pixel in the OFF or white state versus the amount of transmission through the display or pixel in the ON or darkened state.

It is apparent from the above that there exists a need in the art for a normally white liquid crystal display wherein the viewing zone of the display includes high contrast ratios at extended or large vertical and horizontal viewing angles. There also exists a need in the art to center the viewing zone of a NW LCD at a position distant from inversion areas present at or above the 0° vertical viewing axis.

SUMMARY OF THE INVENTION

Generally speaking this invention fulfills the above-described needs in the art by providing a liquid crystal display comprising:

a plurality of pixels, each of these pixels being comprised of a pair of driving electrodes and a twisted nematic liquid crystal material located therebetween, the liquid crystal material being of a thickness "d" and having an anisotropy Δn such that the product of $d \cdot \Delta n$ is about 400–550 nm and wherein the liquid crystal material is capable of twisting at least one normally incident visible wavelength of light passing therethrough in an amount of about 80°–100°;

a rear, light-entrance polarizer having a transmission axis oriented in a first direction;

a front, light-exit polarizer having a transmission axis oriented in a second direction with respect to the first direction thereby to define a normally white display;

a rear retardation film disposed between the rear polarizer and the twisted nematic liquid crystal material;

a front retardation film disposed between the front polarizer and the liquid crystal material; and

wherein the transmission axes of the polarizers and optical axes of the retardation films are so arranged each with respect to the others so as to achieve a white light contrast ratio of at least about 10:1 over a horizontal angular span of at least about 100° and over a vertical angular span of greater than about 55°.

In the preferred forms of this invention contrast ratios of at least about 10:1 over a horizontal angular span of at least about 120° and over a vertical angular span greater than about 60° are achieved; particularly when about 6.0 volts is applied to the display.

In still further preferred forms of this invention the above-described 10:1 contrast ratios are achieved while at the same time 30:1 contrast ratios of at least about 80° over the horizontal angular span and about 30° over the vertical angular span are also achieved. In a particularly preferred form of this invention, furthermore, not only are the above-described ratios achieved but a contrast ratio of about 50:1 is also achieved over a horizontal angular span of about 85° and over a vertical angular span of about 30°. In such embodiments, furthermore, it is preferred to design the display so that the product of

$$\frac{d \cdot \Delta n}{\lambda}$$

is approximately matched to the first minimum of a single, pre-selected color whose wavelength is λ . Such a color is usually red, green, or blue, but may be any other color desired.

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In addition, this invention further fulfills the above-described needs in the art by providing a normally white liquid crystal display including a plurality of pixels comprising: a twisted nematic liquid crystal layer which twists at least one normally incident visible wavelength of light about 80°–100° as it passes therethrough; a first retardation film on a first side of said liquid crystal layer; a second retardation film on a second side of said liquid crystal layer whereby said liquid crystal is disposed between said first and second retardation films; and wherein said first and second retardation films each are uniaxial and have positive or negative retardation values of from about 80–200 nm, and wherein the optical axes of the retardation films are so arranged each with respect to the other so as to achieve a high contrast ratio over a predetermined range of viewing angles.

In certain preferred embodiments of this invention, the first and second retardation films each have an optical axis, and wherein the optical axis of the first retardation film defines a first direction and the optical axis of the second retardation film defines a second direction, and wherein the first and second directions are different by about 75°–100°.

In certain other preferred embodiments of this invention the display further includes a first polarizer substantially adjacent the first retardation film and a second polarizer substantially adjacent the second retardation film, whereby the first and second retardation films are disposed between the first and second polarizers.

In certain further preferred embodiments of this invention the display when about 6.0 volts is applied thereto has a white light contrast ratio of at least about 20:1 at viewing angles of about 0° vertical, $\pm 45^\circ$ horizontal.

In still further preferred embodiments of this invention the display when about 6.0 volts is applied thereto has a white light contrast ratio of at least about 20:1 at viewing angles of about -20° vertical, $\pm 40^\circ$ horizontal.

This invention further fulfills the above-described needs in the art by providing a pixel for a liquid crystal display comprising: a rear, light-entrance polarizer having a transmission axis oriented in a first direction; a front, light-exit polarizer having a transmission axis oriented in a second direction with respect to the first direction thereby to define a normally white pixel; a rear uniaxial retardation film disposed between the rear polarizer and a twisted nematic liquid crystal material, wherein the liquid crystal material twists at least one normally incident visible wavelength of light about 80°–100° as it passes therethrough; a front uniaxial retardation film disposed between the front polarizer and the liquid crystal material; and wherein the front and rear retardation films have positive birefringent values and both have retardation values of from about 80–200 nm, and wherein the transmission axes of said polarizers and optical axes of said retardation films are so arranged each with respect to the others so as to achieve a high contrast ratio over a predetermined range of viewing angles.

In still other preferred embodiments of this invention the pixel has a white light contrast ratio when about 6.0 volts is applied to the pixel of at least about 30:1 at viewing angles of about (i) 0° vertical, -40° horizontal; (ii) 0° vertical, 30° horizontal; (iii) 25° vertical, 0° horizontal; and (iv) -5° vertical, $\pm 25^\circ$ horizontal.

In certain further preferred embodiments of this invention a pixel has a white light contrast ratio when about 6.0 volts is applied to the pixel of at least about 10:1 at viewing angles of about (i) 0° vertical, $\pm 60^\circ$ horizontal; (ii) 30° vertical, 0° horizontal; and (iii) -15° vertical, $\pm 30^\circ$ horizontal.

In certain further preferred embodiments of this invention in angle of from about 80°–100° is defined between the optical axes of the rear and front retardation films. In still

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further preferred embodiments of this invention an angle of from about 85° – 90° is defined between the optical axes of the rear and front retardation films.

This invention further fulfills the above-described needs in the art by providing a liquid crystal display having a viewing zone centered substantially below the 0° vertical viewing axis, comprising: a first polarizer having a transmission axis defining a first direction; a second polarizer having a transmission axis defining a second direction wherein the first and second directions are substantially perpendicular to one another thereby defining a normally white display; a first retardation film having an optical axis and a positive or negative retardation value of from about 80–250 nm; a second retardation film having an optical axis, a twisted nematic liquid crystal layer disposed between the first and second retardation films wherein the liquid crystal layer twists at least one normally incident visible wavelength of light about 80° – 100° as it passes therethrough; wherein the optical axes of the first and second retardation films define an angle δ therebetween of from about 70° – 89° thereby creating a display having its highest contrast viewing zone centered substantially below the 0° vertical viewing axis and remote from inversion areas present above said 0° vertical viewing axis when a voltage of from about 5.0–7.0 volts is applied to the liquid crystal layer.

In certain further preferred embodiments of this invention the angle δ between the optical axes of the rear and front retardation films is from about 75° – 87° thereby positioning and centering the high contrast viewing zone so as to avoid an inversion area of viewing angles located above the 0° vertical axis viewing angle and wherein said retardation films are positively birefringent.

In still further preferred embodiments of this invention the optical axis of the first retardation film and the transmission axis of the first polarizer define an angle θ_1 between the rear retardation film optical axis and the rear polarizer transmission axis of from about 1.5° – 7.5° therebetween.

In still further preferred embodiments of this invention the optical axis of the second retardation film and the transmission axis of the second polarizer define an angle θ_2 between the front retardation film optical axis and the front polarizer transmission axis of from about 1.5° – 7.5° therebetween.

In other preferred embodiments of this invention the angles θ_1 and θ_2 are substantially equal thereby creating a high contrast viewing zone which is substantially symmetrical about the 0° horizontal viewing axis.

This invention further fulfills the above-described needs in the arts by providing a method of shifting the highest contrast viewing zone of a liquid crystal display to a centered position away from an inversion area, comprising the steps of: a) providing the liquid crystal display with a first polarizer having a transmission axis defining a first direction; b) providing the display with a second polarizer having a transmission axis defining a second direction; c) positioning the first and second polarizers on opposite sides of a twisted nematic liquid crystal layer which twists at least one wavelength of normally incident visible light about 80° – 100° when it passes therethrough; d) positioning first and second positively birefringent uniaxial retardation films with substantially equal retardation values on opposite sides of the liquid crystal layer wherein the first retardation film is substantially adjacent the first polarizer, and the second retardation film is substantially adjacent the second polarizer; e) orienting an optical axis of the first retardation film relative to the first polarizer axis so as to define an angle θ_1 therebetween; f) orienting an optical axis of the second retardation film relative to the second polarizer axis so as to

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define an angle θ_2 therebetween; g) selecting values for the θ_1 and θ_2 so as to center the highest contrast viewing zone of the display at a point substantially below the 0° vertical viewing angle axis, thereby positioning and centering the highest contrast viewing zone substantially distant from an inversion area located above the 0° vertical viewing axis.

In certain further preferred embodiments of this invention, the angles θ_1 and θ_2 are selected to be in the range of from about 3° – 5° .

In certain further preferred embodiments of this invention, the angles θ_1 and θ_2 are selected to be in the range of from about 2° – 10° .

In still further preferred embodiments of this invention, the retardation films are uniaxial and have negative birefringence.

In still other preferred embodiments of this invention, the retardation films are biaxial and are either positively or negatively birefringent.

This invention further fulfills the above described needs in the art by providing a pixel for a twisted nematic liquid crystal display, comprising: a rear, light-entrance polarizer having a transmission axis oriented in a first direction; a front, light exit polarizer having a transmission axis oriented in a second direction wherein said first and second directions are substantially perpendicular to one another thereby defining a normally white display; a rear biaxial retardation film disposed between said rear polarizer and a twisted nematic liquid crystal material, wherein the liquid crystal material twists at least one wavelength of normally incident visible light about 80° – 100° as it passes therethrough; a front biaxial retardation film disposed between the front polarizer and the liquid crystal material; wherein the rear retardation film optical axis having the largest index of refraction is oriented in a direction substantially parallel to the first direction of the transmission axis of the rear polarizer, and the front retardation film optical axis having the largest index of refraction is oriented substantially parallel to the second direction of the transmission axis of the front polarizer; and wherein the optical axes of the rear and front retardation films with said largest indices of refraction each have retardation values ($d \cdot \Delta n_{\text{eff}}$) in the range of from about –100 to –200 nm such that the viewing zone of the pixel has high contrast ratios at large predetermined horizontal viewing angles.

This invention will now be described with respect to certain embodiments thereof, accompanied by certain illustrations, wherein:

IN THE DRAWINGS

FIG. 1 is a contrast ratio graph utilizing white light for a light valve liquid crystal pixel with a voltage of 6.8 volts applied thereto.

FIG. 2 is a contrast ratio curve graph using white light in the prior art light valve of FIG. 1.

FIG. 3 is an intensity versus driving voltage plot of the prior art light valve of FIGS. 1 and 2. This plot or graph illustrates a fairly large inversion hump over a wide range of horizontal viewing angles at driving voltages of about 3.2 volts and greater.

FIG. 4 is a schematic diagram of the optical components of a prior art "P-buffed" normally white twisted nematic liquid crystal display having retardation films with retardation values of at least 300 nm.

FIGS. 5A–5D are specific wavelength contrast curve diagrams or graphs showing viewing angle characteristics of the prior art normally white liquid crystal display of FIG. 4.

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Each of the FIGS. 5A-5D represent different orientations of the optical axes of the front and rear polarizers of the FIG. 4 normally white display.

FIG. 6 is a graph illustrating the angular relationship between the horizontal and vertical viewing angles discussed herein, and their relationship with the conventional liquid crystal display angles ϕ and θ .

FIG. 7 is a computer simulation contrast ratio curve graph of a normally white liquid crystal display having front and rear retardation films with retardation values of 320 nm. The display simulated by FIGS. 7-10 is not prior art to the present invention, but is merely used for the purpose of later comparison to certain embodiments of this invention.

FIG. 8 is a computer simulation contrast ratio graph of the display of FIG. 7 wherein 5.0 volts are applied across the display and the 630 nm wavelength is used.

FIG. 9 is a computer simulation contrast ratio curve graph of the display of FIGS. 7-8 using a green wavelength of 550 nm and applying a voltage of 6.8 volts across the liquid crystal material.

FIG. 10 is a computer simulation contrast ratio curve graph of the display of FIGS. 7-9 using a blue wavelength of 480 nm and applying 6.8 volts across the liquid crystal material.

FIG. 11(a) is a schematic diagram of the optical components of a first embodiment of a normally white twisted nematic liquid crystal display of this invention.

FIG. 11(b) illustrates the angular relationships between the respective optical axes of the first embodiment of this invention.

FIG. 11(c) illustrates the angular relationships of another embodiment of this invention as viewed from the point of view of an observer or viewer of the display.

FIG. 12 is a computer simulation contrast ratio curve graph illustrating the contrast ratios of the first embodiment of this invention when 6.8 volts is applied across the liquid crystal material, 120 nm retarders are used, and the red wavelength of 630 nm is used.

FIG. 13 is a computer simulation contrast ratio curve graph of the first embodiment to this invention when 6.0 volts is applied across the liquid crystal material, 120 nm retarders are used, and the red wavelength of 630 nm is used.

FIG. 14 is a computer simulation contrast ratio graph of a display according to the first embodiment of this invention when a green wavelength of 550 nm is used, 120 nm retarders are used, and 6.8 volts is applied across the liquid crystal material.

FIG. 15 is a computer simulation contrast ratio curve graph of the display according to the first embodiment of this invention using a green wavelength of 550 nm when 6.0 volts is applied across the liquid crystal material and 120 nm retarders are used.

FIG. 16 is a computer simulation graph illustrating the contrast ratio curves of the display according to the first embodiment of this invention when a blue wavelength of 480 nm is used and 6.8 volts is applied across the liquid crystal material the rear and front retardation films have retardation values of 120 nm.

FIG. 17 is a computer simulation contrast ratio curve graph illustrating the contrast ratios of a display according to the first embodiment of this invention when a blue wavelength of 480 nm is used, 120 nm retarders are used, and 6.0 volts is applied across the liquid crystal material.

FIG. 18 is a computer simulation transmission versus driving voltage plot of horizontal viewing angles for the first

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embodiment of this invention when the rear and front retardation films have retardation values of 120 nm.

FIG. 19 is a computer simulation transmission versus driving voltage plot of vertical viewing angles for the first embodiment of this invention when the rear and front retardation films have retardation values of 120 nm using white light.

FIG. 20 is a computer simulation contrast ratio curve graph of the first embodiment of this invention when a red wavelength of 630 nm is used, 160 nm retarders are used, and 6.8 volts is applied across the liquid crystal material.

FIG. 21 is a computer simulation contrast ratio curve graph for the first embodiment of this invention when a green wavelength of 550 nm is used, 6.8 volts is applied across the liquid crystal material, and the rear and front retardation films have retardation values of 160 nm.

FIG. 22 is a computer simulation contrast ratio curve graph of the first embodiment of this invention when a blue wavelength of 480 nm is used, 6.8 volts is applied across the liquid crystal material, and the rear and front retardation films have retardation values of 160 nm.

FIG. 23 is a computer simulation contrast ratio curve graph for the first embodiment of this invention when a red wavelength of 630 nm is used, 6.8 volts is applied across the liquid crystal material, and the front and rear retardation films have retardation values of 80 nm.

FIG. 24 is a computer simulation contrast ratio curve graph for the first embodiment of this invention when a green wavelength of 550 nm is used, 6.8 volts is applied across the liquid crystal material, and the rear and front retardation films have retardation values of 80 nm.

FIG. 25 is a computer simulation contrast ratio curve graph of the first embodiment to this invention when a blue wavelength of 480 nm is used, 6.8 volts is applied across the liquid crystal material, and the rear and front retardation films have retardation values of 80 nm.

FIG. 26 is a white light measured contrast ratio curve graph of a light valve according to the first embodiment of this invention which utilized uniaxial and positively birefringent rear and front retardation values of 120 nm, and 6.8 volts was applied to the light valve.

FIG. 27 is a white light measured contrast ratio curve graph of the light valve of FIG. 26 when 6.0 volts was applied to the light valve and uniaxial and positively birefringent rear and front 120 nm retarders were used.

FIG. 28 is a white light measured contrast ratio curve graph of the light valve of FIG. 26 when 5.0 volts was applied thereto, and uniaxial and positively birefringent rear and front 120 nm retarders were used.

FIG. 29 is a white light measured contrast ratio curve graph of the light valve of FIG. 26 when 4.0 volts was applied thereto, and uniaxial and positively birefringent rear and front 120 nm retardation values were used.

FIG. 30 is a white light measured intensity versus driving voltage plot of the light valve of FIG. 26 when rear and front uniaxial and positively birefringent 120 nm retardation films were used. The plot illustrates the gray level behavior of the light valve pixel at a plurality of horizontal viewing angles along the 0° vertical viewing axis.

FIG. 31 is a white light measured contrast ratio curve graph for a normally white liquid crystal display according to the first embodiment of this invention when rear and front 120 nm retardation films were used and 6.8 volts was applied to the display.

FIG. 32 is a white light measured contrast ratio curve graph of the liquid crystal display of FIG. 31 when rear and

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front 120 nm retardation films were used and 6.0 volts was applied to the display.

FIG. 33 is a white light measured contrast ratio curve graph of the liquid crystal display of FIG. 31 when rear and front 120 nm retardation films were used and 5.0 volts was applied to the display.

FIG. 34 is a measured contrast ratio curve graph for the normally white liquid crystal display of FIG. 31 when 4.0 volts was applied to the display, white light was used, and the rear and front retardation films were uniaxial and had retardation values of 120 nm.

FIG. 35 is a measured intensity versus driving voltage plot showing the results for various horizontal angles along the 0° vertical viewing axis for the normally white liquid crystal display of FIG. 31 when white light was used, and the rear and front retardation values were 120 nm.

FIG. 36 is a measured contrast ratio curve graph of a liquid crystal display according to the first embodiment of this invention wherein white light was utilized, 120 nm retarders were used, and 6.0 volts was applied to the display.

FIG. 37 is a measured contrast ratio curve of a light valve according to another embodiment of this invention wherein white light was used, 6.8 volts was applied to the pixel, the retardation films values were 120 nm, and the retardation films were rotated -8° symmetrically.

FIG. 38A is a measured contrast ratio curve of the light valve of FIG. 37 when 5.0 V was applied to the light valve.

FIG. 38B is a white light measured intensity versus voltage graph for the light valve of FIGS. 37 and 38A.

FIG. 39 is a measured contrast ratio curve of a liquid crystal display according to this invention wherein white light was used, 120 nm retardation films were used, 6.0 volts was applied to the display, and the retardation films were rotated -3° symmetrically, and the cell gap "d" was about 5.1 μm in the red subpixel and about 5.7 μm in the green and blue subpixels due to color filter thicknesses.

FIG. 40 is a computer simulation contrast ratio curve graph of a normally white liquid crystal display according to another embodiment of this invention wherein the retardation films are rotated +4° symmetrically, 160 nm retardation films are used, a green 550 nm wavelength is used, and 6.8 V is applied.

FIG. 41 is a cross-sectional view of a liquid crystal display pixel according to certain embodiments of this invention.

FIG. 42 is a partial cut-away view illustrating an active matrix liquid crystal display including a plurality of pixels according to certain embodiments of this invention.

FIG. 43 is a computer simulation contrast ratio curve graph of an LCD according to another embodiment of this invention wherein the rear and front retardation films are uniaxial, but have negative birefringent values. The rear and front retardation films of this embodiment both have retardation values of $\Delta_{xx} = \Delta_{yy} = -160$ nm where $\Delta_{xx} = d(n_x - n_z)$, where "n" is the index of refraction and "d" is the thickness of the film. Therefore, the optical axes of these films are oriented in the "Z" direction.

FIG. 44 is a computer simulation contrast ratio curve graph of an LCD according to yet another embodiment of this invention where the LCD has a cell gap of 5.7 μm , 6.0 V is applied, and the rear and front retardation films are biaxial with negative retardation values. The rear and front films of this embodiment have retardation values Δ_{xx} and Δ_{yy} of -160 nm and -60 nm respectively. A 550 nm wavelength was used in this graph.

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FIG. 45 is a measured contrast ratio graph of a light valve pixel according to another embodiment of this invention where 6.0 V was applied, biaxial rear and front retardation films obtained from Allied Signal Corporation were used, and the light valve was "X-buffed."

DETAILED DESCRIPTION OF CERTAIN EMBODIMENTS OF THIS INVENTION

FIG. 11(a) is a schematic view of the optical components and their respective orientations of a first embodiment of this invention. As shown in FIG. 11(a) the normally white "X-buffed" LCD (or pixel) of this embodiment discloses a rear linear polarizer 1 provided at the light incident side of the liquid crystal layer 5, an exit or front linear polarizer 9 provided at the light exit side of the liquid crystal layer 5, a rear retardation film or plate 3 provided between the liquid crystal layer and the rear polarizer 1, and a front retardation film or plate 7 provided between the liquid crystal layer 5 and the front linear polarizer 9. The retardation films of this embodiment preferably are uniaxial and have positive birefringent (AN) values. An example of uniaxial positively birefringent retardation films useful in the practice of this invention are films commercially available from, for example, Nitto Corp., Japan, or Nitto Denko America, Inc., New Brunswick, N.J. as Model No. NRF-RF120 (120 nm retarder).

In addition, biaxial retardation films are obtainable, for example, from Allied Signal Corporation, and negatively birefringent uniaxial/biaxial soluble polyimide retardation films are obtainable from the University of Akron and may also be used in certain embodiments of this invention.

Normally incident light 11 is directed toward the rear linear polarizer 1 from a conventional backlighting system such as is disclosed, for example, in U.S. Pat. No. 5,161,041. The liquid crystal material 5 is preferably of the twisted nematic type and twists at least one normally incident visible wavelength of light about 80°-100° (most preferably about 90°) as it passes through the liquid crystal layer 5. The amount of twist provided by the liquid crystal layer depends upon: the wavelength of light propagating therethrough, the thickness "d" of the liquid crystal layer 5, the birefringence of the liquid crystal layer, and the orientation of the rear and front buffing zones. The liquid crystal material or layer is preferably about 4.5-6.0 μm thick and has a birefringent value of 0.084 at room temperature.

Between the rear retardation film 3 and the liquid crystal layer 5 is a rear orientation film 21 which has an orientation axis or buffing zone oriented in a direction B_1 . The rear orientation film 21 oriented in direction B_1 acts to align the liquid crystal layer molecules adjacent the rear orientation film in this direction B_1 . The display of FIG. 11(a) is also provided with a front orientation film 22 or buffing zone having an orientation direction B_2 . The direction B_2 of the front orientation film is preferably substantially perpendicular to direction B_1 of the rear orientation film. As is the case with the rear orientation film, the purpose of the front orientation film is to align the liquid crystal molecules along the interface between the liquid crystal layer 5 and the front orientation film in direction B_2 . As described hereinafter more fully, the rear orientation direction B_1 is aligned from the lower right to the upper left, and the front orientation direction B_2 is oriented from the upper right to the lower left which are not to be confused with the directions of the buffing in U.S. Pat. No. 5,134,236 shown in FIG. 4 herein. The effect of the alignment of these two orientation films is to provide for a liquid crystal layer twist of about 80°-100° (most preferably about 90°).

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The rear linear polarizer 1 is arranged so that its transmission axis P_R is substantially parallel with the orientation or buffing direction B_2 of the front orientation film. The front or exit linear polarizer 9 is arranged so that its transmission axis P_F is substantially perpendicular to the transmission axis P_R of the rear linear polarizer 1. Because the transmission axis P_R of the rear linear polarizer 1 is substantially perpendicular to the orientation or buffing direction B_1 of its adjacent orientation film 21, this defines what is meant by "crossed" buffing (i.e. "X-buffed"). "P" (i.e. parallel) buffing simply means that the direction of buffing of the buffing film adjacent its respective polarizer is parallel to the direction of polarization. This arrangement of the transmission axes of the rear and front polarizers also defines a twisted nematic normally white liquid crystal display cell in that as light exits the front linear polarizer 9, it may be viewed by a viewer or observer 15 when the display is in the OFF state.

This embodiment utilizes an "X-buffed" optical arrangement because such an arrangement provides superior results with respect to a "P-buffed" orientation. However, a "P-buffed" arrangement could also be used in certain other embodiments of this invention.

The rear retardation film 3, which is preferably but not necessarily of the uniaxial type, has its optical axis R_R arranged in a direction substantially parallel to the transmission axis P_R of the rear linear polarizer 1. Also, the optical axis R_R of the rear retardation film is arranged in a direction substantially perpendicular to the direction B_1 of the rear orientation film. The retardation value ($d\Delta n$) of the rear retardation film 3 is preferably in the range of about 80–200 nm, more preferably about 100–160 nm, and most preferably about 120–140 nm.

The front and rear retardation films are preferably positioned about equal distances away from the liquid crystal material in this and certain other embodiments of this invention.

The front retardation film 7, which is located on the opposite side of the liquid crystal layer 5 as the rear retardation film 3, is also preferably uniaxial. The optical axis R_F of the front retardation film 7 is preferably oriented in a direction substantially parallel to the transmission axis P_F of the front or exit linear polarizer 9. Also, the optical axis R_F of the front retardation film 7 is preferably oriented in a direction substantially perpendicular to the orientation direction B_2 of the front orientation film. The terms "substantially parallel" and "substantially perpendicular" when used herein but only as used to define the orientation of the optical axes of the rear and front retardation films, means that the axes of the retardation films are arranged in such a manner \pm about 10° unless otherwise specified.

The retardation value of the front retardation film 7 is preferably the same as that of the rear retardation film 3. In other words, the retardation value ($d\Delta n$) of the front retardation film 7 is in the range of about 80–200 nm, more preferably about 100–160 nm and most preferably about 120–140 nm.

The advantages of utilizing about 80–200 nm retardation films according to the teachings of this invention include a resulting larger viewing zone, and the ability to shift the viewing zone vertically away from an inversion area without substantially distorting the viewing zone.

Also, the retardation values of the rear and front retardation films are preferably about the same so as to define a viewing zone substantially symmetrical about the 0° horizontal viewing axis. The greater the difference between the retardation values of the retardation films 3 and 7, the greater

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the loss of symmetry of the viewing zone about the 0° horizontal viewing axis. This may be desirable in certain embodiments of this invention.

Normally incident white light 11 from a conventional backlighting system is directed towards the normally white liquid crystal display shown by FIG. 11(a) and toward the rear linear polarizer 1 and its transmission axis P_R . The rear linear polarizer 1 linearly polarizes the normally incident white light 11 in a direction P_R . After being polarized by the polarizer 1, the light then proceeds toward and through the rear retardation film 3 which has a specific retardation value in the range of about 80–200 nm. After being transmitted through the rear retardation film 3 and being affected by its optical axis R_R , the white light then proceeds through the rear buffing or orientation film having an orientation direction B_1 and into the liquid crystal material 5. When proceeding through the liquid crystal material 5, the twisted nematic material twists the normally incident white light about 80° – 100° , most preferably about 90° .

After exiting the liquid crystal layer 5 (with its molecules aligned along the front surface thereof in direction B_2), the light proceeds through color filters (not shown) and into and through the front retardation film 7. The color filters, may, for example, be red, green, blue, white, or combinations thereof as shown and discussed, for example, in U.S. Pat. No. 4,632,514, the disclosure of which is incorporated herein by reference. After proceeding through the front retardation film 7 and being affected by its optical axis R_F , the color filtered light approaches the front polarizer 9. When the liquid crystal display is in the unenergized or OFF state (no voltage above V_{th} , the threshold voltage, is applied across the liquid crystal material) the twisted light proceeds through the front polarizer 9 and the display appears bright, white, or colored. When the display is in its energized or ON state (a voltage greater than V_{th} is applied across the liquid crystal material) the light is substantially blocked to a voltage dependent extent by the front polarizer 9 and the display appears darkened to a viewer.

Electrodes provided on each side of the liquid crystal material are conventional in the art and are not shown in the drawings of FIGS. 11(a)–11(c) for the purpose of simplicity.

FIG. 11(b) illustrates the angular relationship between the respective axes of the polarizers, retardation films, and orientation films of the first embodiment of this invention. FIGS. 11(b) and 11(c) are perspective views from the viewer side of the liquid crystal display. As shown in FIG. 11(b), the transmission axis P_F of the front polarizer, the optical axis R_F of the front retardation film, and the orientation direction B_1 of the rear orientation film are about parallel one to the others. Also, the transmission axis P_R of the rear polarizer, the optical axis R_R of the rear retardation film, and the direction B_2 of the front orientation film are also about parallel one to the others. Therefore, an angle of about 90° is defined between the orientations of these two groups of directions as shown in FIG. 11(b). Preferably, the angular arrangement shown in 11(b) of the first embodiment of this invention provides for a viewing zone substantially symmetrical about the 0° vertical viewing axis or reader.

The +X and +Y directions are illustrated in FIGS. 11(b) and 11(c), and the +Z direction comes out of the figures toward the viewer or reader.

FIG. 11(c) is a perspective view illustrating the angular relationship between the above discussed optical directions in another embodiment of this invention. In this embodiment, the optical axes of the rear and front retardation films 3 and 7 are symmetrically rotated negatively so as

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to shift the central location of the displays' viewing zone to a position below the 0° vertical viewing axis while substantially preserving its shape. This embodiment of this invention illustrated by FIG. 11(c) utilizes the same parameters as those described with respect to the first embodiment of this invention except for the orientations of the optical axes of the retardation films. As in the first embodiment of this invention, the transmission axes P_r and P_n of the front and rear linear polarizers in this embodiment define an angle of about 90° therebetween. Also, the directions B_1 and B_2 are substantially perpendicular to one another and are about parallel with the transmission axes P_r and P_n of the front and rear polarizers respectively.

The difference between the first embodiment and this embodiment is that in this embodiment shown in FIG. 11(c) the optical axis R_r of the rear retardation film is rotated so as to define an angle θ_1 between the transmission axis of the rear polarizer and the optical axis R_r of the rear retardation film. Also, the optical axis R_n of the front retardation film in this embodiment is rotated so as to define an angle θ_2 between the transmission axis P_r of the front polarizer and the optical axis R_n of the front retardation film.

As illustrated in FIG. 11(c), the optical axis R_n of the rear retardation film is rotated clockwise relative to directions P_n and B_2 , while the optical axis R_r of the front retardation film is rotated counterclockwise relative to directions P_r and B_1 . Preferably, the angles θ_1 and θ_2 as shown in FIG. 11(c) are substantially equal to one another thereby defining a viewing zone for the normally white display which is substantially symmetrical about the 0° horizontal viewing axis. Because the optical axis R_r of the front retardation film has been rotated counterclockwise and the optical axis R_n of the rear retardation film has been rotated clockwise to substantially equal extents, the display of this embodiment is said to have its retardation films rotated negatively in a symmetrical manner. The term "symmetrical" means that the angles θ_1 and θ_2 are substantially equal to one another. For example, if the normally white display illustrated by FIG. 11(c) were to have its rear and front retardation film axes "rotated -8° symmetrically," the angles θ_1 and θ_2 each would be about 4° respectively. Therefore, the angle δ between directions R_n and R_r would be about 82° when the retardation films of this embodiment were rotated -8° symmetrically. It should then be clear that if the optical axes of the rear and front retardation films were to be rotated -4° symmetrically, the angles θ_1 and θ_2 would each be about 2°, and the angle δ between the optical axes of the rear and front retardation films would be about 86°.

The purpose of rotating the optical axes R_n and R_r of the rear and front retardation films is to shift the central location of the viewing zone vertically while still substantially maintaining its shape. In the liquid crystal display art, different customers often desire different viewing characteristics such as the position of the viewing zone. Because of different requirements for different customers, it is advantageous to have a display which may have its viewing zone shifted vertically in accordance with a customer's needs simply by rotating the optical axes of the rear and front retardation films. By rotating the optical axes R_n and R_r of the retardation films to a predetermined negative extent symmetrically, the viewing zone, while being substantially maintained with respect to shape, is shifted to a position centered substantially below the 0° vertical viewing axis and, therefore, away from the inversion zones present above the 0° vertical viewing axis. Such shifts with respect to viewing zones are discussed and shown graphically below with reference to this and other embodiments of this invention.

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Another embodiment of this invention which is related to the embodiment disclosed in FIG. 11(c) is the situation where the optical axes of the rear and front retardation films are rotated to a predetermined positive value symmetrically. When the optical axes R_n and R_r are rotated, for example, +6° symmetrically, the optical axis R_n is rotated 3° counterclockwise relative to directions P_n and B_2 , while retardation axis R_r is rotated 3° clockwise relative to directions B_1 and P_r . Therefore, the rear and front retardation optical axes R_n and R_r define angles θ_1 and θ_2 of about 3° between their axes and the transmission axes of their respective adjacent polarizers. In this situation where the optical axes R_n and R_r are rotated +6° symmetrically, the angle δ is about 96°. When the optical axes of the retardation films are rotated in a positive manner symmetrically, the result is a shifting of the viewing zone to a position centered substantially above the 0° vertical viewing axis.

FIGS. 12-25 are computer simulations of the first embodiment of this invention illustrating the effect of different driving voltages, retardation values, and wavelengths.

FIGS. 12 and 13 are computer simulation contrast ratio curve graphs of the first embodiment of this invention when the red wavelength of 630 nm is used. With respect to FIGS. 12 and 13, the cell gap "d" is 5.70 μm , and the optical axes R_n and R_r of the rear and front retardation films are parallel to the transmission axes of the rear and front linear polarizers respectively. The rear and front retardation films 3 and 7 each have retardation values of 120 nm in the computer simulation graphs of these Figures, as well as FIGS. 14-19.

In FIG. 12, V_{ON} was 6.8 volts and V_{OFF} was 0.9 volts. As can be seen in FIG. 12, the contrast ratios of the red wavelength are extremely good, especially horizontally. The 30:1 contrast ratio curve extends off the graph in both horizontal directions, while the 10:1 contrast ratio curve extends off the graph in the positive vertical direction. The 30:1 contrast ratio curve extends along the 0° vertical viewing axis a total of about 110° from about -55° to +55° horizontal. Furthermore, the 50:1 contrast ratio curve along the 0° vertical viewing axis extends from about -46° to +46°. These are significant improvements over the prior art.

FIG. 13 is a contrast ratio curve graph which used as parameters those described above with respect to FIG. 12 except that V_{ON} was 6.0 volts. As can be seen in FIG. 13, by lowering the parameter V_{ON} or driving voltage, the viewing zone is diminished vertically and is slightly shifted upward in the positive vertical viewing direction. However, when, in FIG. 13, the driving voltage is 6.0 volts, the 50:1 contrast ratio curve extends along the 0° vertical viewing axis to extents of about $\pm 55^\circ$ horizontal.

FIGS. 14-15 are computer simulation contrast (or contour) ratio curve graphs utilizing the green wavelength of 550 nm in the display of the first embodiment of this invention. The cell gap "d" with respect to FIGS. 14-15 was 5.70 μm and the rear and front retardation films 3 and 7 had retardation values of 120 nm. FIG. 14 illustrates the case where V_{ON} was 6.8 volts while FIG. 15 had a V_{ON} of 6.0 volts. As shown in FIG. 14, the 50:1 contrast ratio curve extends horizontally along the 0° vertical viewing axis a total of about 90° from horizontal angles of about -45° to +45°. As can be seen in FIG. 15, by decreasing the driving voltage the viewing zone is constricted slightly vertically and is shifted upward to a position centered substantially above the 0° vertical viewing axis.

FIGS. 16-17 are computer simulation contrast ratio curves of the first embodiment of this invention when the blue wavelength of 480 nm was used and the rear and front

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retardation films had retardation values of 120 nm. In FIGS. 16-17, the cell gap was also 5.70 μm . As was the case with respect to the red and green wavelengths, when V_{ON} is decreased from 6.8 volts (FIG. 16) to 6.0 volts (FIG. 17), the viewing zone shifts upward substantially above the 0° vertical viewing axis and shrinks vertically with respect to the overall vertical angles covered by the 10:1 contrast ratio curve.

FIG. 18 is a driving voltage versus transmission graph illustrating the transmission at various driving voltages in a range of horizontal viewing angles (-60° to 60°) along the 0° vertical viewing axis. With the exception of the $\pm 60^\circ$ curves, there is substantially no effect of inversion upon these transmission versus driving voltage curves throughout the gray level driving voltage zones of about 2-6 volts. In other words, throughout the gray level driving voltage zones, when the driving voltage is increased, the transmission is decreased accordingly, thus, providing for good gray level performance along the 0° vertical viewing axis throughout the horizontal angles shown and defined in FIG. 18. One needs simply to compare the graph of FIG. 18 with the graph of prior art FIG. 3 to see that the arrangements of the optical parameters of the first embodiment of this invention decrease the effect of inversion upon various horizontal viewing angles and provide for an improved gray level performing NW liquid crystal display.

The curves of FIG. 19 representing different vertical viewing angles along the 0° horizontal viewing axis have transmission percentages which generally diminish with increases in driving voltage, possibly with the exception of the +40° vertical viewing angle. The effect of inversion is only seen with respect to the vertical viewing angles of +30° to +40°. In other words, throughout a wide range of gray level driving voltages, when the voltage is increased the transmission is decreased accordingly thus providing for excellent gray level performance throughout the vertical range. The cell gap in FIGS. 18-19 was 5.70 μm . It is noted that while light was used in plotting the driving voltage versus transmission curves of FIG. 18 and FIG. 3. The large inversion humps present in FIG. 3 do not appear in FIGS. 18-19, thus, illustrating an improvement of this embodiment over the prior art.

FIGS. 20-22 are computer simulation contrast ratio curve graphs of the first embodiment of this invention when the rear and front retardation films 3 and 7 had retardation values of 160 nm, V_{ON} was 6.8 volts, and the cell gap "d" was 5.70 μm .

FIG. 20 illustrates the case where the red wavelength of 630 nm was used. In comparing the case where the LCD of the first embodiment utilized 160 nm retardation films (FIG. 20) with the case where 120 nm retardation films (FIG. 12) were used, the difference is that when rear and front retardation values of 120 nm were used the contrast ratios extended to further extents in both the horizontal and vertical directions. For example, with respect to the red wavelength of 630 nm shown in FIG. 12 (120 nm retardation films) and FIG. 20 (160 nm retardation films) the 50:1 contrast ratio curve in FIG. 12 extended horizontally a total of about 110° from about -55° horizontal to about +55° horizontal, while in contrast to this, 50:1 contrast ratio curve in the 160 nm case (FIG. 20) extended horizontally to angles of about $\pm 45^\circ$. However, the boomerang shape of the viewing zone shown in FIG. 12 was substantially eliminated when the 160 nm retardation films were used as shown in FIG. 20. Also, the 30:1 contrast ratio curve in FIG. 20 extended in some places to extents further than that of the 30:1 curve of FIG. 12. In sum, both cases, one with

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retardation films of 120 nm and the other with retardation films of 160 nm, exhibited excellent results in that their respective viewing zones extended to large horizontal and vertical viewing angles.

FIG. 21 illustrates the case where the green wavelength of 550 nm was used in the first embodiment of this invention and the rear and front retardation films 3 and 7 had retardation values of 160 nm. This graph shows that the use of 160 nm retardation films in the first embodiment of this invention provided a viewing zone which extended to large viewing angles in both the horizontal and vertical directions.

FIG. 22 illustrates the case where the blue wavelength of 480 nm was used in combination with 160 nm retardation films. In the cases where 160 nm retardation films were used, the viewing zones were diminished slightly with respect to the 120 nm cases, however, the contrast ratio curves are still excellent.

FIGS. 23-25 are computer simulation contrast ratio curve graphs of the first embodiment of this invention when the rear and front retardation films 3 and 7 had retardation values of 80 nm, V_{ON} was 6.8 volts, and the cell gap "d" was 5.70 μm . FIG. 23 illustrates the case where a red wavelength of 630 nm was used. FIG. 24 illustrates the case where the green wavelength of 550 nm was used, and FIG. 25 illustrates the case where the blue wavelength of 480 nm was used. FIGS. 23-25 all represent excellent contrast ratio curves for the first embodiment of this invention when retardation values of 80 nm were used. The displays of FIGS. 12-25 all utilized uniaxial positively birefringent retardation films.

This invention will now be described with respect to certain examples as follows:

EXAMPLE 1

In this first example, an "X-buffed" light valve having a cell gap "d" of 5.86 μm and a liquid crystal birefringence (Δn) of 0.084 at room temperature was manufactured and tested as follows. The liquid crystal material used is available commercially from E. Merck Ltd. or its U.S. representative EM Industries, Inc., Hawthorne, N.Y. as Model No. ZLI4718. Data resulting from the light valve of this example is illustrated in FIGS. 26-30.

The light valve pixel of this example was similar to the first embodiment of this invention in that the rear linear polarizer had a transmission axis direction about parallel to the optical axis of the rear retardation film, and the optical axis of the front retardation film was about parallel to the transmission axis of the front or exit linear polarizer. The orientation or buffing direction of the rear orientation film was approximately perpendicular to the optical axis of the rear retardation film, and was approximately parallel to the optical axis of the front retardation film. The optical axes of the rear and front retardation films defined an angle δ of about 90° therebetween. The orientation direction of the front orientation film was approximately parallel to the direction of the optical axis of the rear retardation film, and was substantially perpendicular to the direction of the rear orientation film. White light (RGB tri-peaked) was used when testing the light valve of this example (see FIGS. 26-30). The rear and front retardation films were of the uniaxial type and had positive birefringent values. Also, the rear and front retardation films both had retardation values of 120 nm. The temperature was about 35°-40° C.

FIG. 26 illustrates the experimental data when the driving voltage V_{ON} was 6.8 volts and V_{OFF} was 0.2 volts for this example. As can be seen, the 10:1 contrast ratio curve

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extends horizontally along the 0° vertical viewing axis to about ±50° horizontal thereby defining a total horizontal viewing range along the 0° vertical viewing axis of about 100°. This 100° range is to be compared with the about 77° range shown in prior art FIG. 1, and the about 65° horizontal range shown in prior art FIG. 5D. In other words, the 10:1 contrast ratio curve of this example at 6.8 volts is substantially improved over displays and light valves of the prior art. In this respect, it is also to be noted that the 50:1 contrast ratio curve shown in FIG. 26 extends along the 0° vertical viewing axis a substantial distance, i.e. over a total angular span of about 75°.

FIG. 27 illustrates the case where V_{ON} was 6.0 volts for the normally white light valve of this first example. When V_{ON} is decreased from 6.8 volts to 6.0 volts, a more realistic V_{ON} was applied to the pixel and the 10:1 contrast ratio curve extended horizontally slightly further than that shown in FIG. 26.

FIG. 28 illustrates the case where V_{ON} was decreased to 5.0 volts for the light valve of this first example. In the case where 5.0 volts was applied to the pixel, the 10:1 contrast ratio curve defines a range of about 112° along the 0° vertical viewing axis. This is significantly greater than the range defined by the 10:1 contrast ratio curves of the prior art described and illustrated herein.

FIG. 29 illustrates the case where V_{ON} was 4.0 volts for the light valve of this first example. When 4.0 volts was applied to the pixel the 10:1 contrast ratio curve substantially extends off the graph in both horizontal directions. However, when the voltage is decreased, as is the case in FIG. 29, the viewing zone shrinks vertically and is shifted slightly upward, a condition generally true with regard to each of the illustrated decreases in voltage.

FIG. 30 is an intensity versus driving voltage plot for this example illustrating the effects of gray level driving voltages for different horizontal viewing angles ranging from -60° to +60° along the 0° vertical viewing axis. As can be seen in FIG. 30, the gray level performance of this pixel is very good in that the inversion humps are relatively small or non-existent for a wide range of horizontal viewing angles defined herein. In other words, the horizontal gray level performance of this light valve is good because as the driving voltage increases, the intensity for the most part decreases accordingly. Therefore, when the driving voltage of this pixel is increased from one gray level voltage to another the intensity of the pixel generally decreases. The improved results illustrated in the graph shown in FIG. 30 are to be compared to the inferior results illustrated in the prior art graph, FIG. 3, where the inversion humps which begin at about 3.2 volts are relatively large and extend up into the range substantially over 200 fL. In short, the gray level characteristics of the light valve of this example are significantly improved over those of the prior art.

EXAMPLE 2

In this second example, a multi-colored liquid crystal display utilizing TFTs as switching devices in an active matrix array was constructed as follows. The normally white "X-buffed" liquid crystal display had a cell gap "d" of about 5.1 µm for the red subpixel which included a red color filter, and a cell gap "d" of about 5.7 µm for the green and blue subpixels which included green and blue color filters respectively. The difference in cell gap for the different subpixels was due to the different thicknesses of the color filters. The birefringence of the LC material was 0.084 at room temperature. The liquid crystal material was purchased from

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Merck, Model No. ZLI4718. The display had a rear linear polarizer having a transmission axis substantially perpendicular to the transmission axis of the front or exit linear polarizer. A rear retardation film having an optical axis about parallel to the transmission axis of the rear polarizer was sandwiched between the rear polarizer and the liquid crystal material. Likewise, a front retardation film having an optical axis about parallel to the transmission axis of the front polarizer was disposed between the front polarizer and the liquid crystal material. A rear orientation film was provided with an orientation direction about perpendicular to the optical axis of the rear retardation film, and about parallel to the transmission axis of the front polarizer. A front orientation film was provided with an orientation direction substantially parallel to the transmission axis of the rear polarizer, and about perpendicular to the optical axis of the front retardation film.

The optical axes of the rear and front retardation films defined an angle δ of about 90° therebetween. The rear and front retardation films both had retardation values of 120 nm. The front and rear retardation films both had positive birefringent values and were of the uniaxial type purchased from Nitto Denko America Corporation, New Brunswick, N.J. White light was used in testing this display and the measured results are reported in FIGS. 31-35.

FIG. 31 illustrates the contrast ratio curves when a V_{ON} of 6.8 volts was applied to this normally white liquid crystal display. As can be seen, the 10:1 contrast ratio curve extends horizontally along the 0° vertical viewing axis a total of at least about 120°. This range is significantly greater than the ranges defined by the 10:1 contrast ratio curves of the prior art discussed above. Likewise, the 30:1 contrast ratio curve of FIG. 31 extends along the 0° vertical viewing axis to horizontal angles of about ±42° horizontal. The 10:1 contrast ratio curve of this example when 6.8 volts was applied to the display extends vertically along the 0° horizontal viewing axis from about -40° to about +35° vertical. Again, this range defined vertically by the 10:1 contrast ratio curve of this example is significantly improved over that of the prior art.

FIG. 32 illustrates the situation where 6.0 volts was applied to the normally white liquid crystal display of this example. As can be seen in FIG. 32, when 120 nm retardation films are used and 6.0 volts is applied to the display, the 10:1 contrast ratio curve still extends at least a total of about 120° horizontally along the 0° vertical viewing axis. This liquid crystal display clearly exhibits excellent contrast ratio curves over very wide ranges of viewing angles.

FIG. 33 illustrates the situation where 5.0 volts was applied to the display of this example. As shown the 10:1 contrast ratio curve still extends at least a total of about 120° horizontally along the 0° vertical viewing axis when 5.0 volts was applied to the display. The viewing zone, as previously discussed, decreases vertically as the voltage drops.

FIG. 34 illustrates the situation where 4.0 volts was applied to the display of this example. Again, the 10:1 contrast ratio curves still extends off the graph horizontally along the 0° vertical viewing axis defining a range of at least about 120°. Taken together, FIGS. 31-34 illustrate that the inventive normally white display of this example, has excellent contrast ratios over a wide range of driving voltages, especially in the horizontal directions.

FIG. 35 is a driving voltages versus intensity plot for the display of this example when white light was used. This plot is for a range of horizontal viewing angles extending from

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-60° to +60° along the 0° vertical viewing axis. As shown, there is virtually no inversion at any voltage for the various horizontal viewing angles defined therein. In other words, as the gray level or driving voltages increase, the intensity of light emitted from the display decreases in conjunction therewith, thus, providing excellent gray level performance for the display of this example. The plot of FIG. 35 when compared with that of FIG. 3 highlights how the LCDs of this invention virtually eliminate the inversion bumps experienced in the prior art, which allows the displays of this invention to be satisfactorily used throughout a wide range of gray level voltages.

EXAMPLE 3

An "X-buffed" normally white liquid crystal display was constructed having a cell gap of 5.1 μm for the red subpixel including a red color filter, and 5.7 μm for the green and blue subpixels including green and blue color filters respectively. The Δn of the liquid crystal material was 0.084 at room temperature. The liquid crystal material was Merck's Mode No. ZLI4718. This liquid crystal display was driven by a conventional TFT active matrix array.

The normally white display included a rear polarizer, a rear retardation film, a rear substrate, a rear electrode, a rear orientation film, a liquid crystal layer, a front orientation film, a front electrode, a front substrate, a front retardation film, and a front or exit polarizer in that order. The transmission axis of the rear polarizer was approximately parallel to the optical axis of the rear retardation film and the orientation direction of the front orientation film. The transmission axis of the front polarizer was approximately parallel to the optical axis of the front retardation film and the orientation direction of the rear orientation film. The optical axes of the rear and front retardation films defined an angle of about 90° therebetween. The retardation values for both the rear and front films was 120 nm. The rear and front retardation films were of the uniaxial type and had positive birefringent values.

FIG. 36 illustrates the contrast ratio curves for this example when white light was applied to the display and a driving voltage of 6.0 volts was applied. As can be seen, the 10:1 contrast ratio curve extends along the 0° vertical viewing axis to horizontal angles of at least about $\pm 60^\circ$. Also, the 30:1 contrast ratio curve of this example when 6.0 volts was applied to the display extends along the 0° vertical viewing axis to horizontal angles of about $\pm 44^\circ$. These are significant improvements over the prior art. Also, the 10:1 contrast ratio curve as shown in FIG. 36 extends along the 0° horizontal viewing axis to vertical angles of about $\pm 33^\circ$. White light was used in obtaining the data generated by this graph.

EXAMPLE 4

In this example a normally white "X-buffed" light valve according to this invention was constructed wherein the optical axes of the rear and front retardation films were rotated -8° symmetrically thereby shifting the viewing zone to a position centered substantially below the 0° vertical viewing axis while maintaining its shape or integrity.

In this example, the light valve was constructed as follows. A rear linear polarizer was provided with a transmission axis P_r defining a first direction. A front linear polarizer was provided having a transmission axis P_f defining a second direction substantially perpendicular to the first direction. The orientation of the rear orientation film was substantially parallel to the second direction defined by the

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transmission axis P_r of the front polarizer. The orientation direction of the front orientation film was substantially parallel to the transmission axis direction defined by the transmission axis P_r of the rear polarizer.

A rear retardation film of the uniaxial type having a positive birefringent value was disposed between the rear polarizer and the rear orientation film. A front retardation film of the uniaxial type having a positive birefringent value was provided between the front polarizer and the front orientation film.

Because the optical axes of the rear and front retardation films were rotated -8° symmetrically, angles θ_1 and θ_2 were 4° respectively with an angle δ of 82° defining the angle between the optical axes of the rear and front retardation films. In other words, the optical axis R_r of the front retardation film was rotated 4° counterclockwise relative to the transmission axis P_r of the front polarizer. Also, the optical axis R_r of the rear retardation film was rotated clockwise 4° relative to the transmission axis P_r of the rear linear polarizer. Accordingly, the axes of the rear and front retardation films defined an angle of 82° therebetween represented by the angle δ in FIG. 11(c).

The rear and front retardation films of this example had retardation values of 120 nm. The liquid crystal material was Model No. ZLI4718 from E. Merck Ltd. The cell gap "d" of a liquid crystal layer was 5.86 μm for the light valve pixel of this example and the LC birefringence was 0.084. The temperature in this example, as in all of the other examples discussed herein, was about 35° C.-40° C. unless otherwise specified.

FIG. 37 is a contrast ratio curve graph illustrating the viewing zone of the light valve of this example when 6.8 volts and white light was applied thereto. As can be seen, the viewing zone is centered at a position about 10° below the 0° vertical viewing axis (i.e. at about the -10° vertical viewing axis) as a result of the -8° symmetrical rotation of the optical axes of the rear and front retardation films.

This example illustrates the situation where the viewing zone of a display or pixel is shifted to a position substantially below the 0° vertical viewing axis while still substantially maintaining the integrity or symmetry of the overall viewing zone. The symmetry of the viewing zone about the 0° horizontal viewing axis is substantially maintained because the rear and front retardation films had substantially equal retardation values.

FIG. 38A illustrates the viewing zone of the light valve of this example when 5.0 volts and white light was applied thereto. As can be seen in FIG. 38A, the viewing zone is still centered about the -10° vertical viewing axis and is provided with excellent contrast ratios at large viewing angles. As a result of the decrease on V_{on} from 6.8 volts to 5.0 volts, it is seen in FIG. 38A that the viewing zone has been slightly constricted vertically and slightly expanded horizontally about the center of the viewing zone.

The advantage associated with the light valve of this example is that the centered position of the viewing zone of a given liquid crystal display or pixel thereof according to certain embodiments of this invention can be shifted vertically from one position to another while substantially maintaining the symmetry of the viewing zone in accordance with the specific needs of different customers. These shifts of the viewing zone are accomplished by simple rotation, preferably symmetrically, of the optical axes of the rear and front retardation films of certain embodiments of this invention.

FIG. 38B illustrates the inversion hump problem associated with the vertical viewing angles above the 0° vertical

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viewing axis for the display of this example. The viewing zone of the display of this example is centered at a location below the 0° vertical viewing axis remote from these inversion areas illustrated in FIG. 38B. Thus, gray level performance is improved by centering the viewing zone at a position distant the inversion zone thereby limiting inversion effects to remote viewing angles.

EXAMPLE 5

A multi-colored normally white "X-buffed" liquid crystal display was constructed and tested with white light as follows. The display, including a conventional TFT matrix array, included a rear linear polarizer having a transmission axis defining a first direction, a front or exit linear polarizer having a transmission axis defining a second direction wherein the first and second directions were substantially perpendicular to one another, a rear retardation film between the rear polarizer and the liquid crystal layer and having an optical axis substantially parallel to the transmission axis of the rear polarizer, a front retardation film having an optical axis substantially parallel to the transmission axis of the front polarizer, a rear orientation film having an orientation direction substantially perpendicular to the first direction defined by the transmission axis of the rear polarizer, a front orientation film having an orientation direction substantially perpendicular to the transmission axis of the front polarizer, and finally a liquid crystal layer sandwiched between the orientation films. The rear and front retardation films had positive birefringent values and were of the uniaxial type. Furthermore, the rear and front retardation films each had a retardation value of 120 nm.

The optical axes of the rear and front retardation films were rotated -3° symmetrically. Therefore, with reference to FIG. 11(c), angles θ_1 and θ_2 were each 1.5°, and angle δ was 87° in the display of this example.

FIG. 39 is a white light contrast ratio curve graph showing the measured results when the liquid crystal display of this example had a voltage of 6.0 volts applied to the active matrix, V_{OFF} was 0.2 V, and V_{COM} was 8.14 V. The contrast ratios as shown in FIG. 39 are excellent in that the 10:1 contrast ratio curve extends significantly beyond a horizontal range of 120° along the 0° vertical axis. Furthermore, the 30:1 contrast ratio along the 0° vertical viewing axis defines a total range of about 100° which is significantly more than that of the prior art. The 10:1 contrast ratio curve in the vertical direction covers a range along the 0° horizontal viewing axis of between about -20° vertical and at least about 40° vertical.

As can be seen in FIG. 39, the -3° symmetrical rotation of the retardation films was not enough to shift the viewing zone below the 0° vertical viewing angle axis. This may be due to manufacturing derivations associated with certain optical elements of this display. Nevertheless, the viewing zone and contrast ratios are excellent, both horizontally and vertically.

The cell gap "d" of the display manufactured in this example was 5.1 μm in the red subpixel where a red color filter was provided, and 5.7 μm in both the green and blue subpixels where green and blue color filters were provided respectively. The difference in cell gap "d" between the subpixels is a result, as in the other examples herein, of the different thicknesses of the color filters. In other words, because the red color filter has a thickness greater than the green and blue color filters, the cell gap "d" in the red subpixel is less than that in the green and blue subpixels. The LC material birefringence was 0.084 at room temperature. The left handed liquid crystal material was Merck's Model No. ZLI4718.

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EXAMPLE 6

In this example, an "X-buffed" NW light valve pixel was constructed and tested using white light. A rear linear polarizer was provided having a transmission axis defining a first direction and a front linear polarizer was provided having a transmission axis defining a second direction wherein the first and second directions were substantially perpendicular to one another, thus, defining a normally white light valve. A rear retardation film having an optical axis approximately parallel to the transmission axis of the rear polarizer was provided between the rear polarizer and a rear orientation film. The rear orientation film had a buffing or orientation direction substantially parallel to the direction defined by the transmission axis of the front polarizer. A front retardation film having an optical axis about parallel to the transmission axis of the front polarizer was disposed between the front polarizer and a front orientation film. The front orientation film had an orientation or buffing direction substantially perpendicular to that of the rear orientation film.

In this example, the rear and front retardation films were of the biaxial type. Biaxial retardation films can be characterized by two separate retardation values: $d\Delta_{zx}$ and $d\Delta_{zy}$. The local X optical axes of the rear and front biaxial retardation films in this light valve were oriented about parallel to their closest adjacent polarizer transmission axis. The local X axis of a biaxial retardation film herein means the axis in the direction having the highest index of refraction (n_x is always the largest index of refraction and n_z is the lowest). The X, Y, and Z directions (axes) of the biaxial retardation films herein are separate and distinguished from the X, Y, and Z directions (FIG. 6) of the display. In this example, the axis having the retardation value of $d\Delta_{zx} = 168$ nm had the highest or largest index of refraction. Both the rear and front biaxial retardation films were obtained from Allied Signal Corporation as Sample No. 4.0. The indices of refraction of the biaxial retardation films of this example were $n_x = 1.4305$; $n_y = 1.4275$; and $n_z = 1.4261$. The liquid crystal material had a birefringence of 0.084 at room temperature and was Merck's Model No. ZLI4718. The films therefore had retardation values $d\Delta_{zx} = 168$ nm and $d\Delta_{zy} = 53.3$ nm.

FIG. 45 is a contrast ratio curve graph illustrating the measured results of the light valve of this example. In FIG. 45, V_{ON} was 6.0 V and V_{OFF} was 0.2 V. As shown, the 10:1 contrast ratio curve extends horizontally off the graph along the 0° vertical viewing axis, thus, defining a horizontal viewing range of greater than about 120°. Furthermore, the 30:1 contrast ratio curve defines a total viewing range along the 0° vertical viewing axis of about 95°-100°. This is a significant improvement over the prior art. The 10:1 contrast ratio curve in the vertical direction along the 0° horizontal viewing axis covers a range of about 75°.

This example illustrates that when a light valve according to this invention is provided with biaxial rear and front retardation films, excellent viewing zone and contrast ratios result and constitute a significant improvement over the prior art.

EXAMPLE 7

FIG. 40 is a computer simulation contrast ratio curve graph illustrating a simulated liquid crystal display according to another embodiment of this invention where the optical axes of the rear and front retardation films are rotated +4° symmetrically. Due to this positive rotation, the center of the viewing zone is shifted to a position substantially

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above the 0° vertical viewing axis. As shown, the viewing zone of this display is centered about the +20° vertical viewing axis because of the +4° symmetrical rotation of the retardation films.

With reference to FIG. 11(c), the axis R_p of this embodiment is rotated or oriented clockwise relative to P_p and B_p , defining an angle of 2° therebetween. Also, axes R_p of this embodiment is oriented counterclockwise 2° relative to P_p and B_p . As a result, the angle δ between the optical axes of the retardation films is 94° due to the +4° symmetrical rotation of the retardation film axis. The display of this embodiment would be desirable in situations where a viewing zone centered above the 0° vertical viewing axis was desired. The simulation of FIG. 40 used a V_{ON} of 6.8 V, a green wavelength of 550 nm, and 160 nm retarders. The transmission axes of the polarizers as opposed to the optical axes of the retardation films may instead be rotated to shift the location of the viewing zone in certain other embodiments of this invention. However, rotation of the polarizer axes does not provide as good of results as does the rotation of the retarder axes.

EXAMPLE 8

FIG. 43 is a computer simulation of a liquid crystal display according to yet another embodiment of a NW "X-buffed" LCD of this invention. This embodiment is similar to that illustrated and described in the first embodiment of this invention except that the rear and front retardation films 3 and 7 are negatively birefringent and uniaxial. The optical axes of these retardation films are oriented in the "Z" direction, or in other words, in a direction approximately perpendicular to the planes defined by the retardation films. The display of this embodiment, simulated by FIG. 43, had a cell gap of 5.70 μ m, utilized a wavelength of 550 nm in testing the display, a V_{ON} of 6.0 volts, was "X-buffed," and a temperature of about 30° C.

The rear and front retardation films of this embodiment had retardation values of $d\Delta_{ZZ} = d\Delta_{ZZ} = -160$ nm. These films are "uniaxial" because $d\Delta_{ZZ} = d\Delta_{ZZ}$. The retardation value $d\Delta_{ZZ}$ is defined as meaning $d(n_z - n_x)$ where "n" is the index of refraction of a particular axis and "d" is the thickness of the retardation film. The retardation films of this embodiment were negative because the parameter n_x was greater than the parameter n_z . The X, Y, and Z directions of the biaxial retardation films herein are separate and distinguished from the X, Y, and Z directions defining the coordinates of the display.

The term n_x herein always represents the largest index of refraction, and n_z always represents the smallest. The rear and front polarizers had transmission axes which are substantially perpendicular to one another. The rear retardation film was disposed between the rear polarizer and the rear orientation film, and the front retardation film is between the front polarizer and the front orientation film. The negatively birefringent uniaxial retardation films of this embodiment are obtainable from the University of Akron and are disclosed in U.S. Pat. No. 5,071,997 as soluble polyimides and/or copolyimides.

As can be seen in FIG. 43, this embodiment achieves outstanding contrast ratios at very large viewing angles. For example, the 50:1 contrast ratio curve on the 0° vertical viewing axis defines a range of almost 100° horizontally. This is a significant improvement over the prior art.

EXAMPLE 9

FIG. 44 is a computer simulation contrast ratio graph of another NW embodiment of this invention which utilizes

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biaxial front and rear retardation films each having retardation values $d\Delta_{ZZ} = -160$ nm and $d\Delta_{ZZ} = -60$ nm. Because the retardation values are negative, the films have negative birefringence. $d\Delta_{ZZ}$ is defined as $d(n_z - n_x)$ wherein n_x is the largest index of refraction in the film and n_z is the smallest. Therefore, $d\Delta_{ZZ}$ is always the largest retardation value herein. The graph of FIG. 44 was plotted using the parameters of $V_{ON} = 6.0$ volts, a LC birefringence of 0.084, a V_{OFF} of 0.9 V, a cell gap of 5.70 μ m, a temperature of about 30° C., an "X-buffed" configuration, and a wavelength of 550 nm. The local X' is the axis with the largest index of refraction, or n_x . The local X' optical axis of each retardation film is oriented substantially parallel to the adjacent polarizer transmission axis. In other words, the local X' axis of the rear retardation film is substantially parallel to the transmission axis of the rear polarizer, and the local X' optical axis of the front biaxial retardation film is substantially parallel to the front polarizer transmission axis. The local X' optical axis in this embodiment has the aforesaid retardation value of $d\Delta_{ZZ} = -160$ nm, because n_x was the largest index of refraction. The rear and front polarizer axes define an angle of about 90° therebetween. The axis with the smallest index of refraction, or n_z , is oriented about perpendicular to the planes defined by the retardation films. As shown in FIG. 44, the embodiment of this invention using the aforesaid biaxial retardation films achieves excellent contrast ratios at large viewing angles. Again, the 50:1 contrast ratio curve along the 0° vertical viewing axis defines a range of about 100° horizontally.

The specific electrodes and substrates present in the displays and light valves of the above described examples are conventional and were not described or shown for purposes of simplicity.

FIG. 41 is a cross-sectional view of the structural arrangement of a typical liquid crystal display pixel envisioned by this invention. For example, the optical arrangement shown and described in FIGS. 11(a)-11(c) may be used in conjunction with the structural arrangement shown in FIG. 41. Normally incident light enters the pixel and first proceeds through rear linear polarizer 1 and is polarized thereby. After proceeding through the polarizer 1, the normally incident light proceeds through the rear retardation film 3 and the rear transparent substrate 19. The transparent substrates 19 and 20 are preferably made of glass, but also may be made of plastic, quartz, or the like. After proceeding through the rear transparent substrate 19, the light then enters the lower pixel electrode 24 and passes therethrough without being substantially optically affected. The light then proceeds through the rear orientation film 21, a liquid crystal layer 5, the front orientation film 22, and the front electrode layer 25. After proceeding through electrode 25, the light then propagates through the front transparent substrate 20, front retardation film 7, and finally comes to the front or exit linear polarizer 9. When the pixel is in the OFF state, the light proceeds through the linear polarizer 9 toward a viewer. However, when the pixel is in the ON or energized state, the exit polarizer 9 absorbs the light of the pixel and the display appears darkened. Also, color filters (not shown) may be provided at any point between the transparent substrates, and preferably between the front substrate 20 and the electrode layer 25 thereby creating a multicolored pixel including a plurality of colored subpixels. It is understood, of course, that retardation films 3 and 7 may also serve as the buffing layers. In such an embodiment films 3 and 7 are replaced and relocated into the location of buffing films 21 and 22 respectively. It is further understood that retarder films 3 and 7 when not replacing buffing films 21 and 22 may

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be relocated so as to be between their respective driving electrode (24 and 25) and glass substrate (19 and 20) respectively. By arranging the optical elements of this structural arrangement (FIG. 41) as taught by certain optical embodiments of this invention, the aforesaid improved contrast ratios over predetermined ranges of viewing angles may be achieved.

An alternative structural arrangement envisioned by this invention, is a normally white pixel similar to the one shown in FIG. 41, except that the rear and front retardation films 3 and 7 are disposed between the substrates 19 and 20. The rear retardation film is sandwiched between, for example, the rear substrate 19 and the rear electrode 24, and the front retardation film is disposed between the front substrate 20 and the front electrode 25. All embodiments of this invention may be practiced in such a structural arrangement with excellent contrast ratios over a large range of viewing angles being realized.

Furthermore, the retardation films according to certain embodiment of this invention may be personalized or patterned according to the wavelength or color of each subpixel as taught by our commonly owned copending patent application filed Dec. 2, 1993 entitled "Liquid Crystal Display With Patterned Retardation Films," Ser. No. 08/160,731, the disclosure of which is incorporated hereby by reference. In other words, a retardation film within a red subpixel may have a retardation value different than a retardation film in a green or blue subpixel.

FIG. 42 is a partial cut-away view of a typical active matrix liquid crystal pixel array as envisioned by this invention. Herein, the rear and front retardation films, which are not specifically shown in FIG. 42, are sandwiched between their adjacent polarizers 1 and 9, and their adjacent substrates 19 and 20. The individual pixels 30 shown in FIG. 42 are driven by conventional TFTs 31 which act as switching devices to selectively drive each pixel 30. Conventional transparent ITO electrodes 33 connect the individual TFTs 31 to their respective pixels 30. Parallel conductive row lines 35 drive either the gate or drain electrodes of the TFTs 31. Column lines 37 drive the other of the gate and drain electrodes of a TFTs thereby selectively driving the individual pixels 30 when a specific TFT has both its gate and drain electrodes energized.

The simulations, light valves, and displays of FIGS. 7-45 herein were twelve o'clock buffed. Therefore, the rear orientation or buffing directions went from the lower right to the upper left, and the front orientation or buffing direction went from the upper right to the lower left.

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The pretilt angle of the displays, light valves, and simulations of FIGS. 1-3 and 7-45 herein is about 3°, and the value of "d/p" (thickness/natural pitch of the liquid crystal material) of the liquid crystal layer of these Figures is set to about 0.25.

The computer simulations herein were conducted using simulation software written by Dr. Dwight Berreman, Scotch Plains, N.J. The software is described and referenced in one of Dr. Berreman's publications titled "Numerical Modelling of Twisted Nematic Devices," Phil. Trans. R. Soc. Lond. A309, 203-216 (1983) which was printed in Great Britain.

Once given the above disclosure, many other features, modifications, and improvements will become apparent to the skilled artisan. Such other features, modifications, and improvements are, therefore, considered to be a part of this invention, the scope of which is to be determined by the following claims:

We claim:

1. A normally white twisted nematic liquid crystal display comprising:

a liquid crystal layer for twisting at least one normally incident visible wavelength of light from about 80°-100° as it passes therethrough when said liquid crystal layer is in substantially an off state thereby defining a twisted nematic display;

first and second negative biaxial retarders, each of said first and second negative biaxial retarders defined by $n_x > n_y > n_z$, where n_x , n_y , and n_z are respective indices of refraction for each of said biaxial retarders; and

wherein said first negative biaxial retarder has a retardation value $d(n_x - n_y)$ of from about -100 to -200 nm.

2. The normally white display of claim 1, wherein the thickness of said liquid crystal layer is from about 4.5 to 6.5 μm , and the birefringence of said liquid crystal is from about 0.075 to 0.095.

3. The normally white display of claim 2, further comprising a front polarizer and a rear polarizer, wherein a transmission axis of the front polarizer is aligned substantially perpendicular to a transmission axis of the rear polarizer.

4. The normally white display of claim 1, wherein said first and second negative biaxial retarders each are made of a polyimide material.

5. The normally white display of claim 1, wherein said liquid crystal layer has a thickness of from about 4.5 to 6.0 μm .

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